

# DESIGN PRINCIPLES AND CALCULATIONS - NON-COMPOSITE DESIGN

## NON-COMPOSITE DESIGN

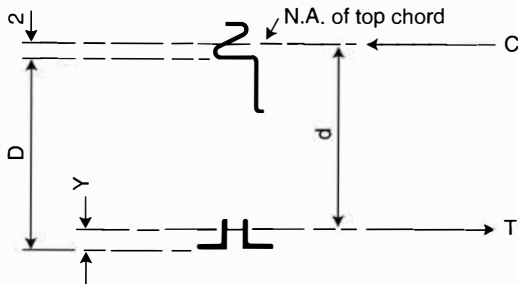


Fig. 4

The top chord must be verified for the loads applied at the non-composite stage. From the previous example, we have the following results:

• Dead load:

Slab 2-1/2 inch: 31 psf  
 Formwork and joist: 5 psf  
 36 psf

• Live load:

Construction live load:  $\frac{20 \times psf}{56 psf}$

\* Reduces beyond 25 foot span at a rate of 1 psf for each 2.5 feet of span.

Moment Capacity of Joist =  $C \times d$  or  $T \times d$

i.e.  $\frac{W_{nc} L^2 \times 12}{8} = C \times d$  or  $T \times d$ , whichever is the lesser

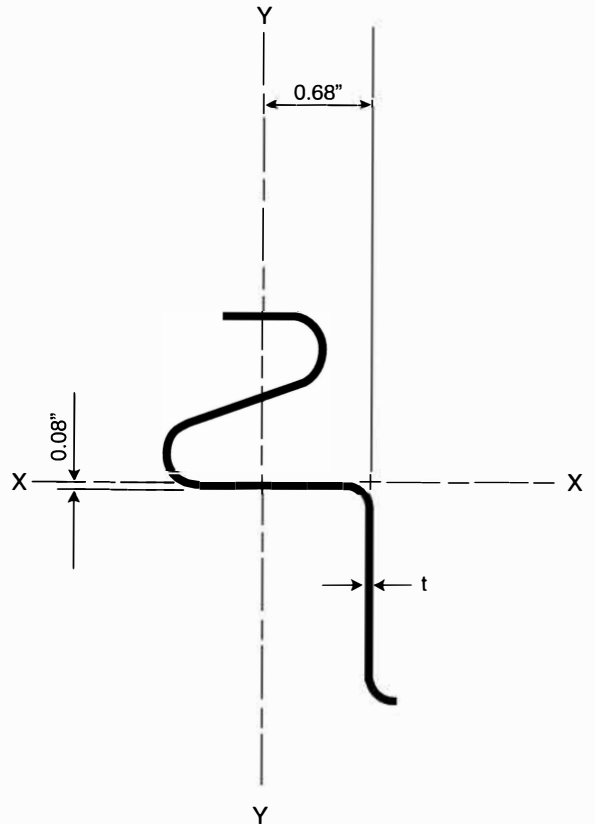
- $W_{nc}$  = 56 x joist spacing =  $plf$
- $L$  = clear span + 4" (ft.)
- $C$  = area of top chord (sq. in.) x working stress (psi)
- $T$  = area of bottom chord (sq. in.) x working stress (psi)
- $d$  = effective lever arm in inches  
 $= D + 0.08 - y$

From the above formula, the maximum "limiting span" may be computed for the non-composite (construction stage) condition. For spans beyond this value, either the top chord must be strengthened or joist propped. Strengthening of the top chord, when required, is usually accomplished by installing one or two rods in the curvatures of the "S" part of the top chord.

The bottom chord is sized for the total factored load which is more critical than the construction load.

Hambro top chord properties are provided to assist you in computing the non-composite joist capacities.

## TOP CHORD PROPERTIES



$$I_x = 0.66 \text{ in.}^4$$

$$\text{Top Chord } S_x = 0.45 \text{ in.}^3$$

$$\text{Bottom Chord } S_x = 0.287 \text{ in.}^3$$

$$L_y = 0.187 \text{ in.}^4$$

$$S_y = 0.167 \text{ in.}^3$$

$$t = 13 \text{ ga.} = 0.090 \text{ in.}$$

$$A_{net} = 0.56 \text{ in.}^2$$

$$= (\text{deducting } 3/8" \text{ deep slot} = 6.25 \times 0.090)$$

$$F_y = 50 \text{ ksi min.}$$

$$F_a = 29.1 \text{ ksi}$$